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**Hydraulic fluid power —  
Determination of pressure ripple  
levels generated in systems and  
components —**

**Part 1:  
Method for determining source flow  
ripple and source impedance of pumps**

*Transmissions hydrauliques — Détermination des niveaux d'onde de  
pression engendrés dans les circuits et composants —*

*Partie 1: Méthode de détermination de l'onde de flux de la source et  
de l'impédance de la source des pompes*



Reference number  
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## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see [www.iso.org/directives](http://www.iso.org/directives)).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received (see [www.iso.org/patents](http://www.iso.org/patents)).

Any trade name used in this document is information given for the convenience of users and does not constitute an endorsement.

For an explanation on the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the WTO principles in the Technical Barriers to Trade (TBT) see the following URL: [Foreword - Supplementary information](#)

The committee responsible for this document is ISO/TC 131, *Fluid power systems*, Subcommittee SC 8, *Product testing*.

This second edition cancels and replaces the first edition (ISO 10767-1:1996), which has been technically revised.

ISO 10767 consists of the following parts, under the general title *Hydraulic fluid power — Determination of pressure ripple levels generated in systems and components*:

- *Part 1: Precision method for pumps*
- *Part 2: Simplified method for pumps*
- *Part 3: Method for motors*

## Introduction

The first edition of ISO 10767-1, published in 1996, was developed with a view to provide means for measurement (experimental determination) of the set of two characteristic values consisting of source flow ripple  $Q_s$  and source impedance  $Z_s$  of hydraulic pumps giving rise to pressure ripple (fluid born vibration) in the hydraulic power circuit., measurement of these two values for a given ripple source is extremely important for design and development of low noise pumps and hydraulic power systems, and for this reason, there is a valid need for such an international standard to experimental measurement of source flow ripple  $Q_s$  and source impedance  $Z_s$ .

However, as discussed in the paragraph below, the so-called “secondary source method” presented in the first edition requires a very complex test system as well as signal processing technique, making its implementation highly difficult; because of this, no country except for the UK, the proposer, has yet adopted ISO 10767-1 as a national standard.

The difficulty can be explained as follows.

To determine the two characteristic values of the source flow ripple,  $Q_s$ , and source impedance,  $Z_s$ , a secondary ripple source is located in the test circuit to generate wide range ripples in the test system. Frequency characteristics of  $Z_s$ , arising from the secondary source, are first determined, followed by measurement of  $Q_s$  of the test pump on the basis of the test pump itself. This means that measurement of the harmonics of the pressure ripple is made with both the test pump and the secondary source in operation. As the result, the measurement accuracy of the harmonic component of the test pump deteriorates significantly as we come close to harmonic frequency level, where differences between the harmonic frequency of the test pump ripple and that of the secondary source become small. To deal with the problem, very complicated signal processing such as compensation is performed, but its practical effect is quite limited. In addition, the standard specifies use of a rotary valve for the secondary source of wide range (50 Hz ~ 4k Hz) ripples, but there is no provision as to the design and frequency characteristics.

These problems arise from the requirement for the secondary source, whereas the method proposed by Weddfelt<sup>[2]</sup> and Kojima<sup>[3]</sup> allows measurement of delivery ripple characteristics ( $Q_s$ ) and the internal source ( $Z_s$ ) on the sole basis of pressure ripple generated by the test pump. This makes the test system quite simple and allows superior accuracy to be achieved without complex processing of signals. The method according to the approaches of Weddfelt and Kojima, respectively, is the same in principle, the only difference between the two being the arrangement of the piping. The present proposal represents the method according to Kojima,<sup>[3]</sup> while annexing that of Weddfelt<sup>[2]</sup> for the purpose of reference.

# Hydraulic fluid power — Determination of pressure ripple levels generated in systems and components —

## Part 1: Method for determining source flow ripple and source impedance of pumps

### 1 Scope

This part of ISO 10767 establishes a test procedure for measuring the source flow ripple and source impedance of positive-displacement hydraulic pumps. It is applicable to all types of positive-displacement pumps operating under steady-state conditions, irrespective of size, provided that the pumping frequency is in the range from 50 Hz to 400Hz.

Source flow ripple causes fluid borne vibration (pressure ripple) and then airborne noise from hydraulic systems. This procedure covers a frequency range and pressure range that have been found to cause many circuits to emit airborne noise which presents a major difficulty in design of hydraulic fluid power systems. Once the source flow ripple and source impedance of hydraulic fluid power pump are known, the pressure ripple generated by the pump in the fluid power system can be calculated by computer simulation using the known ripple propagation characteristics of the system components. As such, this part of ISO 10767 allows the design of low noise fluid power systems to be realized by establishing a uniform procedure for measuring and reporting the source flow ripple and the source impedance characteristics of hydraulic fluid power pumps.

In this part of ISO 10767, calculation is made for blocked acoustic pressure ripple as an example of the pressure ripple. An explanation of the methodology and theoretical basis for this test procedure is given in [Annex B](#). The test procedure is referred to here as the *two pressures/two systems method*. Ratings are obtained as follows:

- a) source flow ripple (in the standard "Norton" model) amplitude, in cubic meter per second[m<sup>3</sup>/s], and phase, in degree, over 10 individual harmonics of pumping frequency;
- b) source flow ripple (in the modified model) amplitude, in cubic meter per second [m<sup>3</sup>/s], and phase, in degree, over 10 individual harmonics of pumping frequency; and its time history wave form,
- c) source impedance amplitude, in Newton second per meter to the power of five [(Ns)/m<sup>5</sup>], and phase, in degree, over 10 individual harmonics of pumping frequency;
- d) blocked acoustic pressure ripple, in MPa (1 MPa = 10<sup>6</sup> Pa) or in bar (1 bar = 10<sup>5</sup> Pa), over 10 individual harmonics of pumping frequency; and the RMS average of the pressure ripple harmonic  $f_1$  to  $f_{10}$ .

### 2 Normative references

The following documents, in whole or in part, are normatively referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 5598, *Fluid power systems and components — Vocabulary*

### 3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 5598 and the following apply.