## Industrial-process control valves - Part 8-3: Noise considerations - Control valve aerodynamic noise prediction method



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# EUROPEAN STANDARD NORME EUROPÉENNE EUROPÄISCHE NORM

## EN 60534-8-3

January 2011

ICS 17.140.20; 23.060.40; 25.040.40

Supersedes EN 60534-8-3:2000

Industrial-process control valves -Part 8-3: Noise considerations ontrol valve aerodynamic noise prediction method (IEC 60534-8-3:2010)

English version

Vannes de régulation des processus industriels -Partie 8-3: Considérations sor le bruit -Méthode de prédiction du bruit aérodynamique des vannes de régulation (CEI 60534-8-3:2010) Stellventile für die Prozessregelung -Teil 8-3: Geräuschbetrachtungen -Berechnungsverfahren zur Vorhersage der aerodynamischen Geräusche von Stellventilen (IEC 60534-8-3:2010)

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#### Foreword

The text of document 65B/765/FDIS, future edition 3 of IEC 60534-8-3, prepared by IEC/SC 65B, Devices & process analysis, of IEC TC 65, Industrial-process measurement, control and automation, was submitted to the IEC-CENELEC parallel vote and was approved by CENELEC as EN 60534-8-3 on 2011-01-01.

This European Standard supersedes EN 60534-8-3:2000.

The significant technical changes with respect to EN 60534-8-3:2000 are as follows:

- predicting noise as a function of frequency;
- using laboratory data to determine the acoustical efficiency factor.

Attention is drawn to the possibility that some of the elements of this document may be the subject of ENELEC shall not be held responsible for identifying any or all such patent patent rights. CEN and rights.

The following dates were

_	latest date by which the EN has to be implemented				
	national standard or by endorsement	(dop)	2011-10-01		
-	latest date by which the national standards conflicting with the EN have to be withdrawn	(dow)	2014-01-01		
An	nex ZA has been added by CENELEC.				
	-2.				
	Endorsement notice				

The text of the International Standard IEC 60534-8-3:20 Was approved by CENELEC as a European Standard without any modification.

In the official version, for Bibliography, the following notes have the added for the standards indicated: A DIED DY TYS

NOTE Harmonized as EN 60534-2-1. [1] IEC 60534-2-1

[2] IEC 60534-8-1 NOTE Harmonized as EN 60534-8-1.

#### Annex ZA

(normative)

# Normative references to international publications with their corresponding European publications

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

NOTE When an international publication has been modified by common modifications, indicated by (mod), the relevant EN/HD applies. **Publication** <u>Title</u> EN/HD Year Yea IEC 60534 Series Industrial-process control valves EN 60534 Series IEC 60534-1 Industrial-process control valves p ontr stions is a preview generated by the openerated by the two the states of the st EN 60534-1 Part Control valve terminology and general considerations

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#### INTRODUCTION

The mechanical stream power as well as acoustical efficiency factors are calculated for various flow regimes. These acoustical efficiency factors give the proportion of the mechanical stream power which is converted into internal sound power.

This method also provides for the calculation of the internal sound pressure and the peak frequency for this sound pressure, which is of special importance in the calculation of the pipe transmission loss.

At present, a common requirement by valve users is the knowledge of the sound pressure level outside the pipe, typically 1 m downstream of the valve or expander and 1 m from the pipe wall. This standard offers a method to establish this value.

The equations in this standard make use of the valve sizing factors as used in IEC 60534-1 and IEC 60534-2-1.

In the usual control valve, the noise travels through the wall of the valve. The noise of interest is only that which travels downstream of the valve and inside of the pipe and then escapes through the wall of the pipe to be measured typically at 1 m downstream of the valve body and 1 m away from the outer pipe wall.

Secondary noise sources may be created where the gas exits the valve outlet at higher Mach numbers. This method allows for the estimation of these additional sound levels which can then be added logarithmically to the sound levels created within the valve.

Although this prediction method cannot surrantee actual results in the field, it yields calculated predictions within 5 dB(A) for the majority of noise data from tests under laboratory conditions (see IEC 60534-8-1). The current edition has increased the level of confidence of the calculation. In some cases the results of the previous editions were more conservative.

The bulk of the test data used to validate the method was generated using air at moderate pressures and temperatures. However, it is believed that the method is generally applicable to other gases and vapours and at higher pressures. Uncertainties become greater as the fluid behaves less perfectly for extreme temperatures and for downstream pressures far different from atmospheric, or near the critical point. The oblations include terms which account for fluid density and the ratio of specific heat.

NOTE Laboratory air tests conducted with up to 1 830 kPa (18,3 bar) upstream pressure and up to 1 600 kPa (16,0 bar) downstream pressure and steam tests up to 225 °C showed good agreement with the calculated values.

A rigorous analysis of the transmission loss equations is beyond the stope of this standard. The method considers the interaction between the sound waves existing in the pipe fluid and the first coincidence frequency in the pipe wall. In addition, the wide tolelances in pipe wall thickness allowed in commercial pipe severely limit the value of the very complicated mathematical approach required for a rigorous analysis. Therefore, a simplified method is used.

Examples of calculations are given in Annex A.

This method is based on the IEC standards listed in Clause 2 and the references given in the Bibliography.

#### INDUSTRIAL-PROCESS CONTROL VALVES -

#### Part 8-3: Noise considerations – Control valve aerodynamic noise prediction method

#### 1 Scope

This part of IEC 00534 establishes a theoretical method to predict the external soundpressure level generated in a control valve and within adjacent pipe expanders by the flow of compressible fluids.

This method considers on single-phase dry gases and vapours and is based on the perfect gas laws.

This standard addresses only the noise generated by aerodynamic processes in valves and in the connected piping. It dee, not consider any noise generated by reflections from external surfaces or internally by pipe fittings, mechanical vibrations, unstable flow patterns and other unpredictable behaviour

It is assumed that the downstream provide is straight for a length of at least 2 m from the point where the noise measurement is mage.

This method is valid only for steel and stee vy pipes (see Equations (21) and (23) in 5.5).

The method is applicable to the following single stage valves: globe (straight pattern and angle pattern), butterfly, rotary plug (eccentric, spherical), ball, and valves with cage trims. Specifically excluded are the full bore ball valves where the product  $F_pC$  exceeds 50 % of the rated flow coefficient.

For limitations on special low noise trims not covered by this standard, see Clause 8. When the Mach number in the valve outlet exceeds 0,3 for standard trim or 0,2 for low noise trim, the procedure in Clause 7 is used

The Mach number limits in this standard are as follows:

	Mach number limit			
Mach number location	Clause 5 Standard trim	Clause 6 Noise-reducing trim	Clause 7 High Mach number applications	
Freely expanded jet M <sub>j</sub>	No limit	No limit	<b>OR</b> o limit	
Valve outlet M <sub>o</sub>	0,3	0,2	1,0	
Downstream reducer inlet M <sub>r</sub>	Not applicable	Not applicable	1,0	
Downstream pipe M <sub>2</sub>	0,3	0,2	0,8	

#### 2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies. IEC 60534-1, Industrial-process control valves – Part 1: Control valve terminology and general considerations

#### 3 Terms and definitions

For the purposes of this document, all of the terms and definitions given in the IEC 60534 series and the following apply:

3.1

## acoustical efficiency

 $\eta$  ratio of the stream power converted into sound power propagating downstream to the stream power of the mass flow

#### 3.2

#### external coincidence frequency

f<sub>g</sub>

frequency at which the external acoustic wavespeed is equal to the bending wavespeed in a plate of equal thickness to the pipe wall

#### 3.3

#### internal coincidence frequency

f<sub>o</sub>

lowest frequency at which the internal acoustic and structural axial wave numbers are equal for a given circumferential mode, thus resulting in the minimum transmission loss

#### 3.4

#### fluted vane butterfly valve

butterfly valve which has flutes (grooves) on the Gace(s) of the disk. These flutes are intended to shape the flow stream without altering the Gating line or seating surface

#### 3.5

#### independent flow passage

flow passage where the exiting flow is not affected by the exiting flow from adjacent flow passages

#### 3.6

#### peak frequency

f<sub>p</sub>

frequency at which the internal sound pressure is maximum

#### 3.7

#### valve style modifier

Fd

ratio of the hydraulic diameter of a single flow passage to the diameter of a circular orifice, the area of which is equivalent to the sum of areas of all identical flow passages at a given travel

